

IN THE CLAIMS

1. - 3 (canceled)

4. (currently amended) ~~A designing~~ In a method of designing an acoustic matching layer or layers of a piezoelectric transducer including a piezoelectric plate that is an electric device of a ceramic group capable of converting an electric pulse into a sound wave pulse signal, a back absorption layer that is a sound wave absorption layer for preventing an echo phenomenon of the piezoelectric plate, one or more of the acoustic matching layers ~~formed in that~~ is a thin layer structure constructed in order that sound waves generated in the piezoelectric plate can be transferred in the direction of a front load, and an electric matching device that is an electric device for matching an external electric equipment and electric impedance, ~~so that the present invention is well adapted to various fields such as medical diagnosis, underwater detection, nondestructive evaluation, etc., an optimum designing method of matching layers of a thickness mode piezoelectric transducer, the improvements~~ comprising the steps of:

(1) a step in which a ~~certain~~ front load effective impedance is inputted, and a sensitivity, pulse width and performance index of a piezoelectric transducer are computed based on a KLM model computation;

(2) a step in which a minimum value of a front load effective impedance is selected based on a sensitivity, pulse width and performance index of the piezoelectric transducer computed in the step (1);

(3) a step in which a the selected minimum value of the front load effective impedance is inserted into ~~the matching formula shown in the following table obtained based on the following formula; and~~

~~(4) a step in which an impedance computed in the step (3) is determined as an impedance of each layer,~~

{formula}

$$\ln \frac{Z_{i+1}}{Z_i} = 2^{-n} C_i^n \ln \frac{Z_t}{Z_f^{(0)}}$$

where $i = 0, \dots, n$, $Z_0 = (Z_f)^{(0)}$, $Z_{n+1} = Z_t$, $C_i^n = \frac{n!}{(n-i)!i!}$, and

$$C_i^n = \frac{n!}{(n-i)!i!}$$

; and

(4) a step in which an impedance computed in the step (3) is determined as an impedance Z_1, Z_2, Z_3 of each of the matching layers according to the following Table

{Table}

| Impedance | Z_1 | Z_2 | Z_3 |
|------------------|------------------------------|------------------------------|------------------------------|
| Number of layers | | | |
| 1 | $((Z_f)^{(0)} (Z_t))^{1/2}$ | | |
| 2 | $(Z_f)^{(0)3/4} (Z_t)^{1/4}$ | $(Z_f)^{(0)1/4} (Z_t)^{3/4}$ | |
| 3 | $(Z_f)^{(0)7/8} (Z_t)^{1/8}$ | $(Z_f)^{(0)} (Z_t)^{1/2}$ | $(Z_f)^{(0)1/8} (Z_t)^{7/8}$ |

where Z_f represents an effective impedance of front load viewed from the front side of the piezoelectric plate, and $(Z_f)^{(0)}$ is (Z_f) at the free resonant frequency, and (Z_t) is a front load impedance, and the above results are obtained until for a number n of the matching layers $n=1, 2$ or 3 , wherein a video waveform, not a RF waveform, is used for evaluating the sensitivity and pulse width of the piezoelectric transducer.

5. (new) In a method of designing a piezoelectric transducer including a piezoelectric plate of a ceramic group for converting an electric pulse into a sound wave pulse signal, a back sound wave absorption layer for preventing an echo phenomenon of the piezoelectric plate, and one to three acoustic matching layers having respective impedances (Z_1, Z_2, Z_3) so that sound waves generated in the piezoelectric plate can be transferred in the direction of a front load, the improvements comprising:

selecting a front load impedance (Z_t) and an effective impedance of the front load (Z_f) viewed from a front side of the piezoelectric plate; and

determining the impedances (Z_1, Z_2, Z_3) of each of the acoustic matching layers using the following matching formula and table:

$$\ln \frac{Z_{i+1}}{Z_i} = 2^{-n} C_i^n \ln \frac{Z_t}{Z_f^{(0)}}$$

, where $i = 0, \dots, n$, $Z_0 = (Z_f)^{(0)}$, $Z_{n+1} = Z_t$,

$$C_i^n = \frac{n!}{(n-i)! i!}$$

and

[Table]

| Impedance | Z_1 | Z_2 | Z_3 |
|------------------|------------------------------|------------------------------|------------------------------|
| Number of layers | | | |
| 1 | $((Z_f)^{(0)} (Z_t))^{1/2}$ | | |
| 2 | $(Z_f)^{(0)3/4} (Z_t)^{1/4}$ | $(Z_f)^{(0)1/4} (Z_t)^{3/4}$ | |
| 3 | $(Z_f)^{(0)7/8} (Z_t)^{1/8}$ | $(Z_f)^{(0)} (Z_t)^{1/2}$ | $(Z_f)^{(0)1/8} (Z_t)^{7/8}$ |

where Z_f represents the effective impedance of front load viewed from the front side of the piezoelectric plate, and $(Z_f)^{(0)}$ is (Z_f) at the free resonant frequency, and (Z_t) is the front load impedance, and the above results are obtained.